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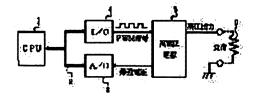
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(54) POWER SUPPLY EMPLOYING PWM CONTROL SYSTEM

(57)Abstract:

PURPOSE: To obtain a power supply excellent in rising characteristics and steady characteristics by employing different output voltage control factors at the time of rising and during steady operation.

CONSTITUTION: An I/O interface 4 is connected with a high voltage power supply 5 generating a different high voltage depending on the pulse duty of a PWM signal and an output from the high voltage power supply 5 is applied to a load 6. The output voltage from the high voltage power supply 5 is stepped down and fed, as a feedback voltage signal, to an A/D converter 3. When the difference between a feedback voltage and a target feedback voltage is sufficiently small. the value of an output voltage control factor (OC) is equalized to a basic gain by a CPU 1 using an acceleration gain regulating constant.



When the square of the difference exceeds the acceleration gain

regulating constant, the acceleration gain increases over 2 and the OC varies depending on the product of acceleration gain and basic gain. The acceleration gain varies gradually in the region where the difference is relatively small and the variation increases as the difference increases.

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Industrial Application] This invention relates to the power unit using the PWM control system which started the power unit which used the PWM control system, especially made good the both sides of a rising characteristic and a stationary characteristic.

[0002]

[Description of the Prior Art] The power unit using PWM control as equipment which generates the conventional, for example, direct current, high voltage is known. This type of power unit has the description that control of output voltage is easy and tends to stabilize output voltage. It is desirable to define a factor for output voltage control (control gain) which is satisfied with the power unit using this PWM control system of each of the rising characteristic immediately after an injection of an electric power switch and the stationary characteristic after predetermined time passes, and to perform armature-voltage control.

[0003]

[Problem(s) to be Solved by the Invention] However, it could necessarily be satisfied with neither of power unit using the conventional PWM control system of both the properties of a rising characteristic and a stationary characteristic. That is, the rising characteristic was getting worse, although the stationary characteristic became good when the value of the factor for output voltage control was conversely made small by a stationary characteristic worsening, although the rising characteristic became good when the value of the factor for output voltage control was enlarged.

[0004] Then, it is made in order that this invention may solve such a technical problem, and a rising characteristic and both the properties of a stationary characteristic set it as the purpose of each invention to offer the power unit using a good PWM control system.

[0005]

[Means for Solving the Problem] In the power unit using the PWM control system which performs armature-voltage control which makes an actual output voltage value in agreement with a target electrical-potential-difference value in invention according to claim 1 using the factor for output voltage control in an PWM control system It has a 1st armature-voltage control means to change and control said factor for output voltage control by the time of a standup until it reaches said target direct-current-voltage value, and the stationary after reaching said target electrical-potential-difference value, and the 1st purpose is attained. It has a 2nd armature-voltage control means to start from the time of a stationary, to sometimes enlarge said factor for output voltage control, and to control by invention according to claim 2, and the 2nd purpose is attained.

[0006] In invention according to claim 3, a target electrical-potential-difference value is compared with the fed-back actual output voltage value, it has a 3rd armature-voltage control means to control an output voltage value using the factor for output voltage control called for based on this comparison result, and the 3rd purpose is attained. In invention according to claim 4, said 3rd armature-voltage control means attains the 4th purpose by enlarging the factor for output voltage control and controlling it, so that the difference of said target electrical-potential-difference value and the fedback actual output voltage value is large.

[0007]

[Function] With the power unit using an PWM control system according to claim 1, the 1st armature-voltage control means changes the factor for output voltage control, and controls output voltage by the time of a standup until it reaches a target electrical-potential-difference value, and the stationary after reaching said target electrical-potential-difference value. The 2nd armature-voltage control means starts, makes the factor for output voltage control at the time larger than the factor for output voltage control at the time of a stationary, and controls output voltage by the power unit using an PWM control system according to claim 2. The 3rd armature-voltage control means compares the desired

value of the electrical-potential-difference value which a power unit generates with the electrical-potential-difference value which said fed-back power unit generated, asks for the factor for output voltage control based on this comparison result, and controls output voltage by the power unit using an PWM control system according to claim 3. Said 3rd armature-voltage control means enlarges the factor for output voltage control, and controls output voltage by the power unit using an PWM control system according to claim 4, so that the difference of said target electrical-potential-difference value and feedback voltage value is large. [0008]

[Example] Hereafter, one example in the power unit using the PWM control system of this invention is explained to a detail with reference to drawing 1 thru/or drawing 5. The bus line 2 which consists of a data bus etc. is connected to CPU1 which is the "1st and 3rd armature-voltage control means" as shown in drawing 1, and the I/O interface 4 which sends out the PWM signal generated by CPU1 is connected with A/D converter 3 which changes into a digital signal the feedback voltage signal (feedback signal) explained to the degree which consists of an analog signal at the bus line 2. The I/O interface 4 is connected to the high-voltage power source 5 which generates the high voltage which changes with magnitude of the pulse duty of an PWM signal, and the high-voltage output outputted from the high-voltage power source 5 is impressed to a load 6. The electrical potential difference generated with the high-voltage power source 5 is decompressed, and is inputted into A/D converter 3 as a feedback voltage signal.

[0009] Next, actuation of the example constituted in this way is explained.

** The main routine of the control algorithm which generates the PWM signal for performing armature-voltage control processing to main routine drawing 2 is shown. When there are no activation directions of armature-voltage control processing, the output of an PWM signal is forbidden (step 1;Y), an electrical-potential-difference PWM phase angle timer value is made into the minimum value, the output of armature-voltage control PWM is turned OFF (step 5), and processing is ended. In step 1, when there are activation directions of armature-voltage control processing, an PWM signal is outputted (step 1; N), and when timing (control timing) for electrical-potential-difference PW modification processing to control by already ending is not suitable, (step 2; N) and processing are ended. Moreover, in step 2, electrical-potential-difference PW modification processing is unsettled, when control timing is suitable, it recognizes that (step 2;Y) electrical-potential-difference PW modification processing was completed (step 3), when target electrical-potential-difference data are "0", a (step 4;Y) electrical-potential-difference PWM phase angle timer value is made into the minimum value, the output of armature-voltage control PWM is turned OFF (step 5), and processing is ended. In step 4, when target electrical-potential-difference data are not "0", the subroutine (armature-voltage control PW value modification processing) shown in (step 4; N) and drawing 3 is performed (step 6), and processing is ended. The above processing is processing at the time of directions of armature-voltage control processing activation. [0010] ** The flow chart of a subroutine (armature-voltage control PW value modification processing) is shown in subroutine (armature-voltage control PW value modification processing) drawing 3. This subroutine is an algorithm which calculates the updating value of an electrical-potential-difference PWM phase angle timer. As shown in drawing 3, a feedback electrical-potential-difference value is beyond a target feedback electrical-potential-difference value (step 11;Y), when a feedback electrical-potential-difference value is larger than a target feedback electrical-potentialdifference value, the difference of (step 12; N), a feedback electrical-potential-difference value, and a target feedback electrical-potential-difference value is calculated (step 13), and the subroutine (count of an armature-voltage control PW control input) shown in drawing 4 is performed (step 14). And the count result of an armature-voltage control PW control input is added to an old electrical-potential-difference PWM phase angle timer value (step 15). However, an electrical-potential-difference PWM phase angle timer value is restricted to an armature-voltage control PW upper limit (step 16), and ends processing so that maximum of an armature-voltage control PW value may not be exceeded. [0011] Moreover, in step 11, when a feedback electrical-potential-difference value is smaller than a target feedback electrical-potential-difference value, the difference of (step 11; N), a feedback electrical-potential-difference value, and a target feedback electrical-potential-difference value is calculated (step 17), and the subroutine (count of an armaturevoltage control PW control input) shown in drawing 4 is performed (step 14). And the count result of an armaturevoltage control PW control input is subtracted from an old electrical-potential-difference PWM phase angle timer value (step 18). However, an electrical-potential-difference PWM phase angle timer value is restricted to an armature-voltage control PW lower limit (step 19), and ends processing so that it may not become under the minimum value of an armature-voltage control PW value.

[0012] ** a subroutine (count of an armature-voltage control PW control input) -- this subroutine -- the difference of a feedback electrical-potential-difference value and a target feedback electrical-potential-difference value -- it is the algorithm which was made to enlarge the value of the factor for output voltage control, so that a value is large. difference -- "1" is added to the value which squared the value (= feedback electrical-potential-difference value-target feedback electrical-potential-difference value), and divided the result by the acceleration gain tone integer constant,

and the acceleration gain of armature-voltage control is searched for (step 21). This acceleration gain searched for is made below into the maximum of the acceleration gain of armature-voltage control, and prepares a upper limit (step 22). subsequently, the value which multiplied the calculated acceleration gain value by basic gain (= acceleration gain / difference value) (step 23), and was further calculated at step 23 -- difference -- it multiplies by the value and considers as the value of an electrical-potential-difference PW control input (step 24). The minimum value of the calculated armature-voltage control PW control input is restricted in a upper limit (step 25), and PW value and PW control input are memorized (step 26).

[0013] namely, -- according to this algorithm -- a steady state -- difference -- when a value is sufficiently small, with an acceleration gain tone integer constant, the operation of step 21 is set to "1" and the value of the factor for output voltage control becomes equal to the value of basic gain. difference -- if the square of a value serves as a value more than an acceleration gain tone integer constant, acceleration gain will become two or more values, and the factor for output voltage control will also change based on the value of the product of acceleration gain and basic gain. acceleration gain -- difference -- since it is calculated based on the square operation of a value -- difference -- the field where a value is comparatively small -- acceleration gain -- **** -- changing -- difference -- the amount of value changes of acceleration gain also becomes large as a value becomes large.

[0014] Therefore, in a steady state, fine control is possible, when the time of the standup of an electrical potential difference and desired value are changed, the factor for output voltage control changes dynamically, and the time amount to which output voltage reaches a target electrical potential difference becomes short. Moreover, also when output voltage shifts from a target electrical potential difference, PW value is controlled by the proper factor value for output voltage control according to the value shifted by disturbance etc., and it can return to a target electricalpotential-difference value early according to it. the difference at the time of making the upper limit of an acceleration gain tone integer constant, basic gain, and acceleration gain, and the upper limit of PW control input into a proper value at drawing 5 -- the relation of the control input of the acceleration gain over a value and PW value is shown. Drawing 5 (a) shows relation when an acceleration gain tone integer constant is set to 16 and it sets [basic gain] the upper limit of 10 and PW control input to 255 for the upper limit of 1/8 and acceleration gain. Moreover, drawing 5 (b) shows relation when an acceleration gain tone integer constant is set to 4 and it sets [basic gain] the upper limit of 8 and PW control input to 255 for the upper limit of 1/8 and acceleration gain. for example, it is shown in drawing 5 (a) -- as -- the difference of a target electrical potential difference and a feedback electrical potential difference -- case a value is large -- (for example, 50) the factor for output voltage control -- large -- carrying out (acceleration gain being set as 6) -- said difference -- when a value is small (for example, 10), the factor for output voltage control is made small (acceleration gain is set as 1). [0015]

[Effect of the Invention] As explained above, according to invention according to claim 1, start, are changing the factor for output voltage control in the time and the time of a stationary, and according to invention according to claim 2 Start from the time of a stationary, sometimes enlarge the factor for output voltage control, and according to invention according to claim 3 Since it asks for the factor for output voltage control based on the comparison with desired value and a feedback value, and according to invention according to claim 4 the factor for output voltage control is enlarged so that the difference of desired value and a feedback value is large The power unit which was excellent in the property at the time of a property and a stationary at the time of a standup can be offered.

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CLAIMS

[Claim(s)]

[Claim 1] The power unit using the PWM control system characterized by to have a 1st armature-voltage-control means change and control said factor for output-voltage control by the time of a standup until it reaches said target electrical-potential-difference value, and the stationary after reaching said target electrical-potential-difference value in the power unit using the PWM control system which performs armature-voltage control which makes an actual output-voltage value in agreement with a target electrical-potential-difference value using the factor for output-voltage control.

[Claim 2] The power unit using the PWM control system according to claim 1 which starts said factor for output voltage control from the time of a stationary, and is characterized by having a 2nd armature-voltage control means to sometimes enlarge and to control.

[Claim 3] The power unit using the PWM control system according to claim 1 characterized by having a 3rd armature-voltage control means to control an output voltage value using the factor for output voltage control which compared the target electrical-potential-difference value with the fed-back actual output voltage value, and was called for based on this comparison result.

[Claim 4] Said 3rd armature-voltage control means is a power unit using the PWM control system according to claim 3 characterized by enlarging the factor for output voltage control and controlling it, so that the difference of said target electrical-potential-difference value and the fed-back actual output voltage value is large.

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DESCRIPTION OF DRAWINGS

[Brief Description of the Drawings]

[Drawing 1] It is the block diagram of the example of this invention.

[Drawing 2] It is the Maine flow chart of armature-voltage control processing of said example.

[Drawing 3] It is the subroutine of the armature-voltage control PW value modification processing in said Maine flow chart.

[Drawing 4] It is the subroutine of count of the armature-voltage control PW control input in said Maine flow chart. [Drawing 5] It is drawing showing the control input of PW value over the difference in said example, and the relation of acceleration gain. (a) acceleration gain tone integer constant; -- the case where it is referred to as 16, basic gain; 1/8, upper-limit; 10 of acceleration gain, and upper-limit; 255 of PW control input -- it is -- (b) -- acceleration gain tone integer constant; -- it is the case where it is referred to as 4, basic gain; 1/8, upper-limit; 8 of acceleration gain, and upper-limit; 255 of PW control input.

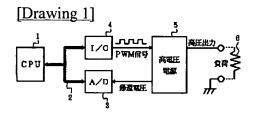
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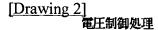
- 1 CPU (the 1st 3rd Armature-voltage Control Means)
- 3 A/D Converter
- 4 I/O Interface
- 5 High-Voltage Power Source
- 6 Load

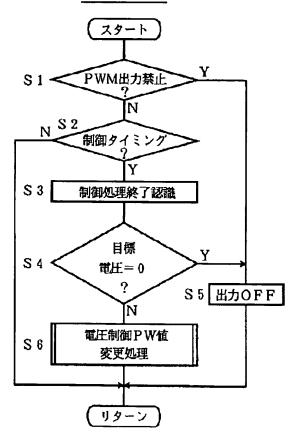
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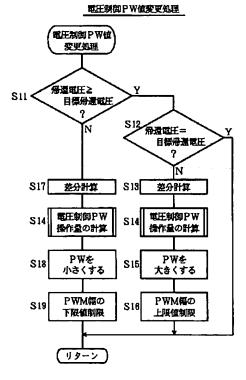
DRAWINGS

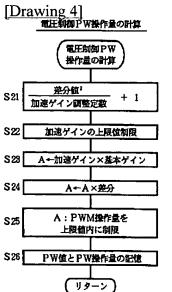




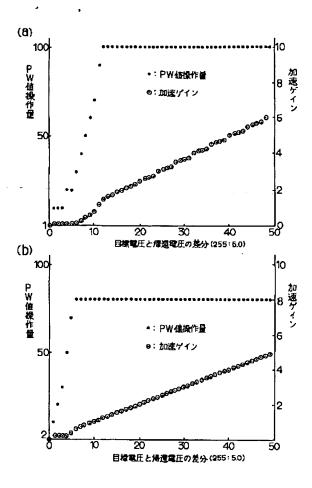


[Drawing 3]





[Drawing 5]



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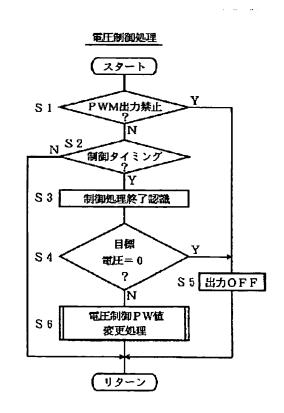
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(54) 【発明の名称】 PWM制御方式を用いた電源装置

(57)【要約】

【目的】 立上り時特性および定常時特性の両方に優れたPWM制御方式を用いた電源装置を提供する。

【構成】 PWM制御方式を用いた電源装置において、目標電圧値と帰還電圧値との差が大きい程、制御ゲインを大きくすることにより、立上り時特性と定常時特性の両方を満足させる。



【特許請求の範囲】

【請求項1】 出力電圧制御用の因子を用い、現実の出力電圧値を目標電圧値に一致させる電圧制御を行うPW M制御方式を用いた電源装置において、

前記目標電圧値に達するまでの立上り時と、前記目標電 圧値に達した後の定常時とでは、前記出力電圧制御用因 子を変えて制御する第1電圧制御手段を備えたことを特 徴とするPWM制御方式を用いた電源装置。

【請求項2】 前記出力電圧制御用因子を、定常時よりも立上り時に大きくして制御する第2電圧制御手段を備えたことを特徴とする請求項1記載のPWM制御方式を用いた電源装置。

【請求項3】 目標電圧値と、フィードバックされた現実の出力電圧値とを比較し、この比較結果に基づいて求められた出力電圧制御用因子を用いて出力電圧値を制御する第3電圧制御手段を備えたことを特徴とする請求項1記載のPWM制御方式を用いた電源装置。

【請求項4】 前記第3電圧制御手段は、前記目標電圧値とフィードバックされた現実の出力電圧値との差が大きい程、出力電圧制御用因子を大きくして制御することを特徴とする請求項3記載のPWM制御方式を用いた電源装置。

【発明の詳細な説明】

[0001]

【産業上の利用分野】本発明は、PWM制御方式を用いた電源装置に係り、特に立上り特性および定常特性の双方を良好にしたPWM制御方式を用いた電源装置に関する。

[0002]

【従来の技術】従来、例えば、直流高電圧を発生する装置としてPWM制御を用いた電源装置が知られている。このタイプの電源装置は、出力電圧の制御が容易であり、出力電圧を安定化し易いという特徴を有している。このPWM制御方式を用いた電源装置では、電源スイッチを投入直後の立上り特性と、所定時間が経過した後の定常特性とのそれぞれを満足するような出力電圧制御用の因子(制御ゲイン)を定めて電圧制御を行うことが好ましい。

[0003]

【発明が解決しようとする課題】しかし、従来のPWM制御方式を用いた電源装置では、必ずしも立上り特性と定常特性の両特性を共に満足することができなかった。すなわち、出力電圧制御用因子の値を大きくすると、立上り特性は良くなるものの、定常特性が悪くなり、逆に、出力電圧制御用因子の値を小さくすると、定常特性は良くなるものの、立上り特性が悪くなっていた。

【0004】そこで、本発明はこのような課題を解決するためになされたものであり、立上り特性および定常特性の両特性が良好なPWM制御方式を用いた電源装置を提供することを各発明の目的とする。

[0005]

【課題を解決するための手段】請求項1記載の発明では、PWM制御方式における出力電圧制御用の因子を用い、現実の出力電圧値を目標電圧値に一致させる電圧制御を行うPWM制御方式を用いた電源装置において、前記目標直流電圧値に達するまでの立上り時と、前記目標電圧値に達した後の定常時とでは、前記出力電圧制御用因子を変えて制御する第1電圧制御手段を備えて第1目的を達成する。請求項2記載の発明では、前記出力電圧制御用因子を、定常時よりも立上り時に大きくして制御する第2電圧制御手段を備えて第2目的を達成する。

2

【0006】請求項3記載の発明では、目標電圧値と、フィードバックされた現実の出力電圧値とを比較し、この比較結果に基づいて求められた出力電圧制御用因子を用いて出力電圧値を制御する第3電圧制御手段を備えて第3目的を達成する。請求項4記載の発明では、前記第3電圧制御手段は、前記目標電圧値とフィードバックされた現実の出力電圧値との差が大きい程、出力電圧制御用因子を大きくして制御することにより第4目的を達成する。

[0007]

【作用】請求項1記載のPWM制御方式を用いた電源装 置では、第1電圧制御手段が、目標電圧値に達するまで の立上り時と、前記目標電圧値に達した後の定常時とで は、出力電圧制御用因子を変えて出力電圧を制御する。 請求項2記載のPWM制御方式を用いた電源装置では、 第2電圧制御手段が、立上り時の出力電圧制御用因子 を、定常時の出力電圧制御用因子よりも大きくして出力 電圧を制御する。請求項3記載のPWM制御方式を用い た電源装置では、第3電圧制御手段が、電源装置が発生 する電圧値の目標値と、フィードバックされた前記電源 装置が発生した電圧値とを比較し、この比較結果に基づ いて出力電圧制御用因子を求め、出力電圧を制御する。 請求項4記載のPWM制御方式を用いた電源装置では、 前記第3電圧制御手段が、前記目標電圧値とフィードバ ック電圧値との差が大きい程、出力電圧制御用因子を大 きくして出力電圧を制御する。

[0008]

【実施例】以下、本発明のPWM制御方式を用いた電源 装置における一実施例を図1ないし図5を参照して詳細 に説明する。図1に示すように、「第1および第3電圧 制御手段」であるCPU1にはデータバス等からなるバスライン2が接続され、バスライン2にはアナログ信号 からなる次に説明する帰還電圧信号(フィードバック信号)をデジタル信号に変換するA/D変換器3と、CPU1で生成されたPWM信号を送出する1/Oインターフェース4が接続されている。I/Oインターフェース4は、PWM信号のパルスデューティの大きさによって 異なる高電圧を発生する高電圧電源5に接続され、高電 圧電源5から出力された高電圧出力が負荷6に印加され

る。高電圧電源5で発生された電圧は、減圧されて帰還 電圧信号としてA/D変換器3に入力される。

【0009】次に、このように構成された実施例の動作について説明する。

①メインルーチン

図2に、電圧制御処理を行うためのPWM信号を生成す る制御アルゴリズムのメインルーチンを示す。電圧制御 処理の実行指示がない場合にはPWM信号の出力を禁止 し(ステップ1;Y)、電圧PWM位相角タイマ値を最 小値とし、電圧制御PWMの出力をオフにして(ステッ プ5)、処理を終了する。ステップ1において、電圧制 御処理の実行指示がある場合には PWM信号を出力し (ステップ1;N)、電圧PW変更処理が既に終了し制 御をするためのタイミング(制御タイミング)が適当で ない場合には(ステップ2;N)、処理を終了する。ま た、ステップ2において、電圧PW変更処理が未処理で 制御タイミングが適当な場合には(ステップ2;Y)、 電圧PW変更処理が終了したことを認識し(ステップ 3)、目標電圧データが「0」の場合には(ステップ 4; Y)、電圧 PWM位相角タイマ値を最小値とし、電 20 圧制御PWMの出力をオフにして(ステップ5)、処理 を終了する。ステップ4において、目標電圧データが 「O」でない場合は(ステップ4;N)、図3に示すサ ブルーチン(電圧制御PW値変更処理)を実行し(ステ ップ6)、処理を終了する。以上の処理が、電圧制御処 理実行の指示時の処理である。

【 0 0 1 0 】 ②サブルーチン(電圧制御 P W値変更処理)

図3に、サブルーチン(電圧制御PW値変更処理)のフローチャートを示す。このサブルーチンは、電圧PWM 10位相角タイマの更新値を求めるアルゴリズムである。図3に示すように、帰還電圧値が目標帰還電圧値以上であり(ステップ11;Y)、帰還電圧値が目標帰還電圧値とり大きい場合には(ステップ12;N)、帰還電圧値と目標帰還電圧値との差分を計算し(ステップ13)、図4に示すサブルーチン(電圧制御PW操作量の計算)を実行する(ステップ14)。そして、電圧制御PW操作量の計算結果を今までの電圧PWM位相角タイマ値に加算する(ステップ15)。但し、電圧制御PW値の最大値を越えないように、電圧PWM位相角タイマ値は電大値を越えないように、電圧PWM位相角タイマ値は電圧制御PW上限値に制限し(ステップ16)、処理を終了する。

【0011】また、ステップ11において、帰還電圧値が目標帰還電圧値より小さい場合には(ステップ11: N)、帰還電圧値と目標帰還電圧値との差分を計算し(ステップ17)、図4に示すサブルーチン(電圧制御PW操作量の計算)を実行する(ステップ14)。そして、電圧制御PW操作量の計算結果を今までの電圧PWM位相角タイマ値から減算する(ステップ18)。但し、電圧制御PW値の最小値未満にならないように、電 50

圧PWM位相角タイマ値は電圧制御PW下限値に制限し (ステップ19)、処理を終了する。

【 0 0 1 2 】 <u>③サブルーチン(電圧制御 P W操作量の計</u> 算)

このサブルーチンは、帰還電圧値と目標帰還電圧値との差分値が大きい程、出力電圧制御用因子の値を大きくするようにしたアルゴリズムである。差分値(=帰還電圧値ー目標帰還電圧値)を二乗してその結果を加速ゲイン調整定数で割った値に「1」を加え、電圧制御の加速ゲインを求める(ステップ21)。この求めた加速ゲインは、電圧制御の加速ゲインの最大値以下とし上限値を設ける(ステップ22)。次いで、求めた加速ゲイン値に基本ゲイン(=加速ゲイン/差分値)を掛け算し(ステップ23)、更にステップ23で求めた値に差分値を掛け算して電圧PW操作量の値とする(ステップ24)。求めた電圧制御PW操作量の最小値を上限値内に制限し(ステップ25)、PW値とPW操作量を記憶する(ステップ26)。

【0013】すなわち、このアルゴリズムによると、定常状態で差分値が十分小さい場合には、加速ゲイン調整定数によってステップ21の演算は「1」となり、出力電圧制御用因子の値は基本ゲインの値と等しくなる。差分値の二乗が加速ゲイン調整定数以上の値となると、加速ゲインは2以上の値となって、出力電圧制御用因子も加速ゲインと基本ゲインの積の値に基づいて変化する。加速ゲインは、差分値の二乗演算に基づいて計算されるので、差分値が比較的小さい領域では、加速ゲインは除々に変化し、差分値が大きくなるにつれて、加速ゲインの値の変化量も大きくなっていく。

【0014】従って、定常状態においては、細かい制御 が可能で、電圧の立上り時や目標値を変更した場合に は、ダイナミックに出力電圧制御用因子が変化して、出 力電圧が目標電圧に到達する時間が短くなる。また、外 乱等によって、出力電圧が目標電圧からずれた場合に も、そのずれた値に応じた適正な出力電圧制御用因子値 でPW値が制御され、目標電圧値に早く戻すことができ る。図5に、加速ゲイン調整定数、基本ゲイン、加速ゲ インの上限値、PW操作量の上限値を適宜の値とした場 合における、差分値に対する加速ゲインおよびPW値の 操作量の関係を示す。図5(a)は、加速ゲイン調整定 数を16、基本ゲインを1/8、加速ゲインの上限値を 10、PW操作量の上限値を255とした場合の関係を 示す。また、図5(b)は、加速ゲイン調整定数を4、 基本ゲインを1/8、加速ゲインの上限値を8、PW操 作量の上限値を255とした場合の関係を示す。例え ば、図5(a)に示すように、目標電圧と帰還電圧の差 分値が大きい場合には(例えば、50)、出力電圧制御 用因子を大きくし(加速ゲインを6に設定)、前記差分 値が小さい場合には(例えば、10)、出力電圧制御用 因子を小さくしている(加速ゲインを1に設定)。

[0015]

【発明の効果】以上説明したように、請求項1記載の発明によれば、立上り時と定常時とで出力電圧制御用因子を変えており、請求項2記載の発明によれば、出力電圧制御用因子を、定常時よりも立上り時に大きくし、請求項3記載の発明によれば、目標値とフィードバック値との比較に基づいて出力電圧制御用因子を求め、請求項4記載の発明によれば、目標値とフィードバック値との差が大きい程、出力電圧制御用因子を大きくしているので、立上り時特性および定常時特性に優れた電源装置を提供することができる。

【図面の簡単な説明】

【図1】本発明の実施例のブロック図である。

【図2】前記実施例の電圧制御処理のメインフローチャートである。

【図3】前記メインフローチャートにおける電圧制御P

W値変更処理のサブルーチンである。

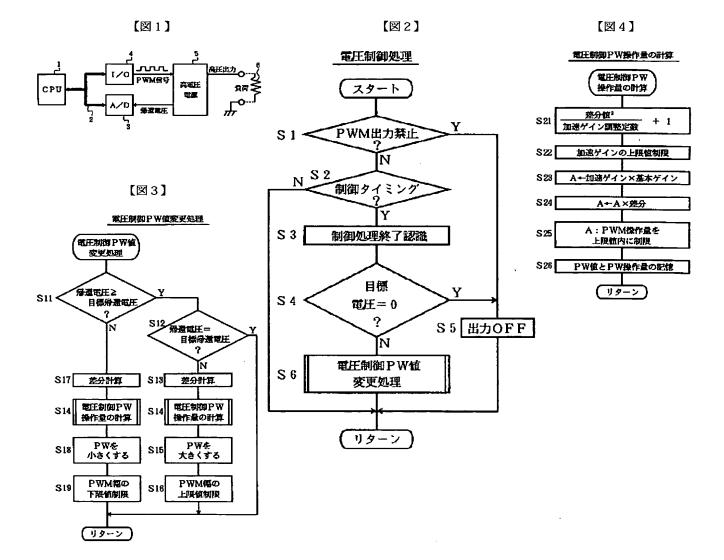
【図4】前記メインフローチャートにおける電圧制御P W操作量の計算のサブルーチンである。

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【図5】前記実施例における差分に対するPW値の操作量および加速ゲインの関係を示す図であって、(a)は、加速ゲイン調整定数;16、基本ゲイン;1/8、加速ゲインの上限値;10、PW操作量の上限値;255とした場合であり、(b)は、加速ゲイン調整定数;4、基本ゲイン;1/8、加速ゲインの上限値;8、PW操作量の上限値;255とした場合である。

【符号の説明】

- 1 CPU(第1~第3電圧制御手段)
- 3 A/D変換器
- 4 1/0インターフェース
- 5 高電圧電源
- 6 負荷



【図5】

